



## **Section 2.0 Principles of Wood Design**

FEMA US&R Response Sys/U.S. Army Corps of Engineers  
US&R Structure Specialist Training – StS1



**SECTION 2.0**  
**Principles of Timber Design**

Oct08

### **Introduction**

- Wood is the primary material for providing temporary shoring during US&R operations.
- Timber design not always part of the structural engineering curriculum.
- Module introduces the principles of timber design and how they relate to US&R shoring.

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### **Timber Design Specifications**



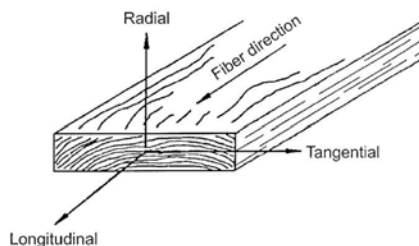
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### **Wood**

- **Non-Homogeneous** – primary component comprised of bonded elongated glucose monomers that form the cell walls of wood.
- **Orthotropic** – wood has unique and independent mechanical properties in the directions of three mutually perpendicular axis.
- **Anisotropic** – wood exhibits different mechanical properties when measured along different axes.

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### **Wood - Anisotropic**



USDA Forest Service Wood Handbook, 1999

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### **Trees**

Given all the different varieties, trees can still be dividing into two broad classes:

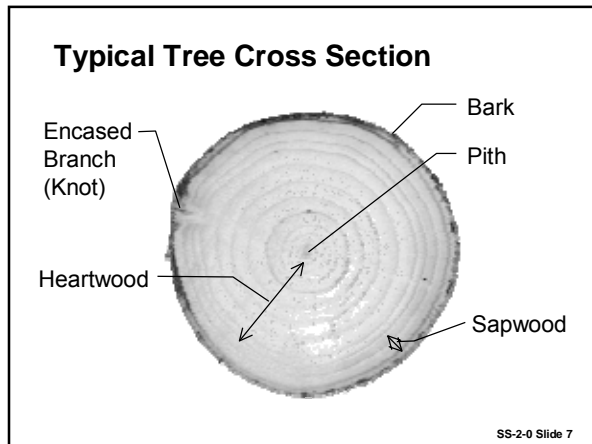
- Hardwoods
- Softwoods

Hardwoods – Deciduous trees. Seeds are enclosed in the a flower. Broad leaves.

Softwoods – Coniferous trees. Cone-bearing (seeds are exposed) with needle-like or scale-like evergreen leaves.

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## **Section 2.0 Principles of Wood Design**



### **Sapwood**

- Mechanism for water and sap transport.
- Contains both living and dead cells.
- Greater portion of the wood in second-growth trees.

### **Heartwood**

- Consists of inactive cells.
- Does not assist in water and sap transport.
- May be darker in color than softwood due to extractive content.

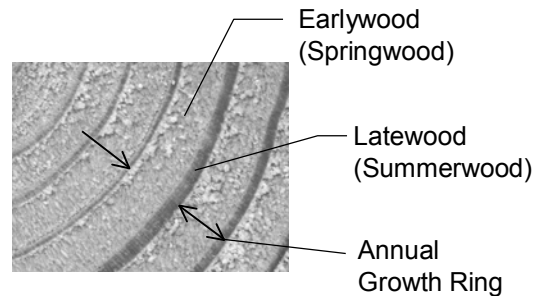
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### **Growth Rings**

- A familiar characteristic of a tree or log cross section.
- Also referred to as *Annual Rings*.
- Found in trees that grow in temperate climates so that distinct yearly growing seasons occur.
- Inner portion of the growth ring forms first in the growing season and is called *Earlywood*.
- Outer portion of the growth ring forms later in the growing season and is called *Latewood*.

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### **Growth Rings**



### **Earlywood**

- Fast growing (also referred to Springwood).
- Cells with relatively large cavities and thin walls.
- Less dense and weaker than Latewood.

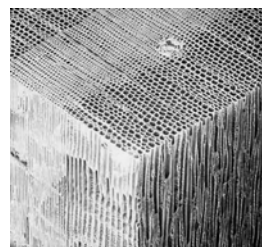
### **Latewood**

- Slow growing (also referred to Summerwood).
- Cells with relatively small cavities and thick walls.
- More dense and stronger than Earlywood.

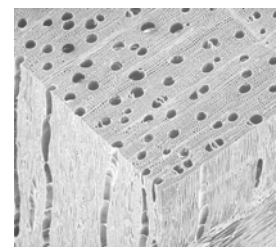
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### **Cell Structure of Wood**

#### **Softwood**



#### **Hardwood**



(Society of Wood Science And Technology )

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## Section 2.0 Principles of Wood Design

### Water

- Water of a living tree can make up  $\frac{2}{3}$  of its total weight.
- Water is contained in wood as either bound water or free water.
- Bound water is held within cell walls by bonding forces between water and cellulose molecules.
- Free water is contained in the cell cavities and is not held by bonding forces (like water in a pipe.)

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### Drying of Wood

- Structural wood must be dried to reduce its moisture content to an acceptable level for the end user.
- Drying results in an increase in strength and stiffness.
- Drying results in a volume change as the cell wall shrink (shrinkage).
- General Drying processes: Air and Kiln.

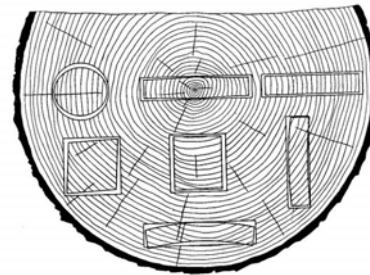
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### Shrinkage

- Wood is dimensionally unstable when moisture content is reduced below its Fiber Saturation Point (FSP) or Green state (approx. 25%).
- Occurs as moisture is removed (seasoning).
- Degree dependent on orientation with grain: tangential, radial, and longitudinal.
  - Tangential = shrink abt 1/3% for each 1% moisture
  - Radial = shrink abt 1/5% for each 1% moisture
  - Longitudinal = Nil for D. Fir & So. Pine
- Results in defects due to grain separation.

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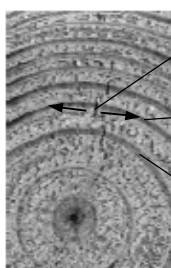
### Shrinkage



USDA Forest Service Wood Handbook, 1999

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### Tangential Shrinkage

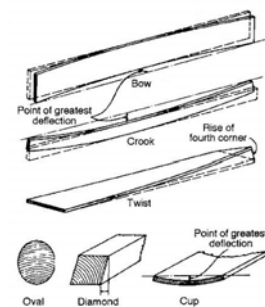


Tangential Shrinkage Crack (Check)  
 Local Direction of Maximum Shrinkage  
 Annual Rings

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### Warping

Differential shrinkage caused by differences in radial, tangential, and longitudinal shrinkage is a major cause of warp.



USDA Forest Service Wood Handbook, 1999

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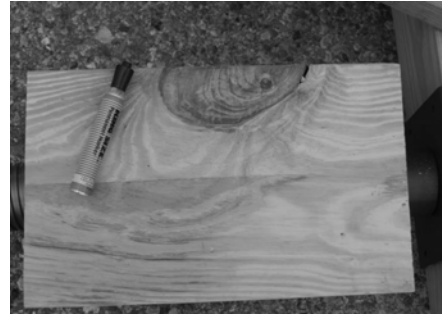
## **Section 2.0 Principles of Wood Design**

### **Factors Affecting Wood Strength and Behavior**

- Wood Species
- Moisture Content
- Growing Defects such as Knots and Checks
- Shrinkage Cracks
- Wood Grain Orientation (slope of grain)
- Growth Rate (rings per inch)

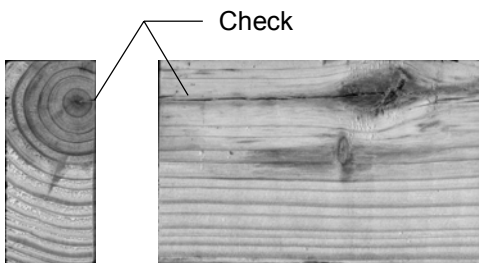
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### **Knots**



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### **Checks**



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### **Slope of Grain**

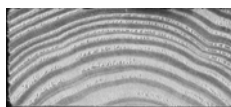
<u>Slope of Grain</u>	<u>% of Retained Strength</u>
0	100%
1 in 20	93%
1 in 10	81%
1 in 5	55%

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### **Growth Rings Per Inch**



Fast Growing  
Lower Strength



Slow Growing  
Higher Strength

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### **Additional Factors Affecting Strength**

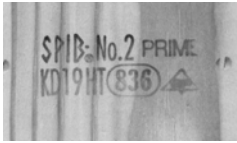
- Decay
- Heartwood and Sapwood
- Shakes
- Wane
  - (see FOG5 Sect 5 Glossary)
- Reaction Wood

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## **Section 2.0 Principles of Wood Design**

### **Grading**

Appearance Grading



Based on size and distribution of defect

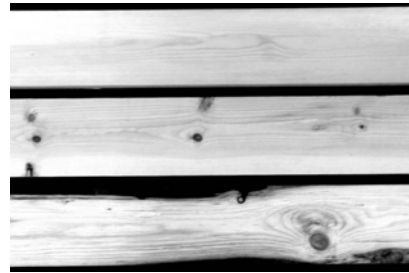
Stress Grading



Based on measured relationship between load and deflection

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### **Visual Grading (Southern Pine)**



No. 1

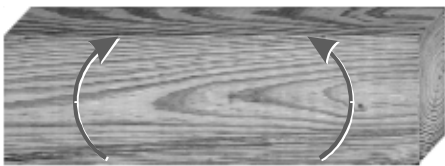
No. 2

No. 3

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### **Extreme Fiber in Bending, $F_b$**

$F_b$  (Compression)

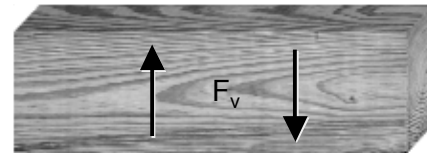


$F_b$  (Tension, Controls)

Strength base on Modulus of Rupture.

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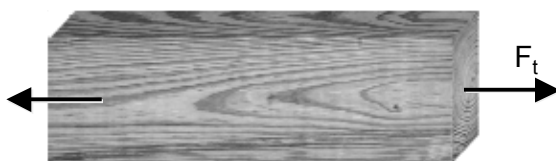
### **Flexural Shear, $F_v$**



NDS-2001 increased the allowable shear values for all species by approximately 100 percent.

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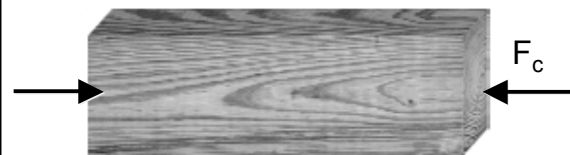
### **Tension, $F_t$**



Not much test data. Usually  $F_b$  is modified.

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### **Compression, $F_c$**

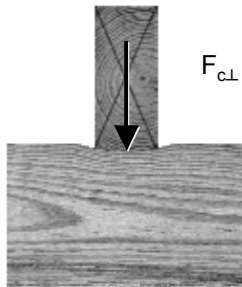


Length to least cross sectional dimension of less than 11. Otherwise, stability issues.

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## Section 2.0 Principles of Wood Design

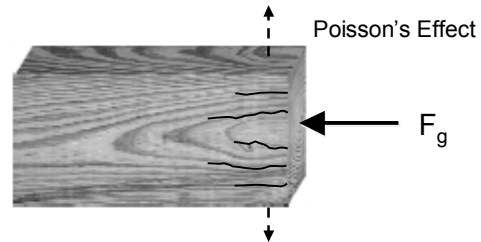
### Compression Perpendicular to Grain, $F_{c\perp}$



Weak stress orientation but very ductile  
 650 psi for post bearing  
 500 psi for cribbing (due to exaggerated deflections)

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### End Grain In Bearing, $F_g$



Replaced by  $F_c$  NDS-2001.

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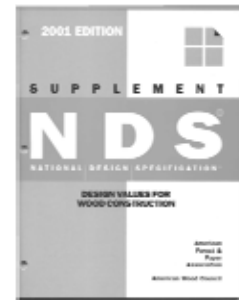
### Modulus of Elasticity, E

- Differs with respect to orientation with grain.
- $E_L$  – Longitudinal direction (bending stiffness, deflection), tabulated value.
- $E_T$  – Tangential and  $E_R$  – Radial are between 0.01 and 0.10 of  $E_L$ .

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### NDS Supplement

In addition to other information, such as cross sectional properties, the NDS Supplement provides the tabulated allowable stress values for different species of wood and their grades.



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### NDS Supplement – Allowable Stresses

USE WITH TABLE 4A ADJUSTMENT FACTORS

Species and commercial grade	Size classification	Design values in pounds per square inch (psi)					Modulus of Elasticity E	Building Code Agency
		Bending $F_b$	Tension parallel to grain $F_t$	Shear parallel to grain $F_v$	Compression parallel to grain $F_c$	Compression perpendicular to grain $F_{c\perp}$		
<b>DOUGLAS FIR-LARCH</b>								
Select Structural	2" x 4" thick	1500	900	95	425	1700	1,900,000	N/A
No. 1 & 2		1200	800	85	325	1500	1,800,000	
No. 3		1000	675	80	225	1300	1,700,000	
No. 4	2" x 6" wider	800	575	75	125	1100	1,600,000	
Boards		600	475	70	125	900	1,500,000	
Common		500	400	65	125	800	1,400,000	
Timber		400	325	60	125	700	1,300,000	
<b>DOUGLAS FIR-LARCH (SOFT)</b>								
Select Structural	2" x 4" thick	1300	875	90	425	1500	1,900,000	N/A
No. 1 & 2		1000	775	85	325	1300	1,800,000	
No. 3		800	675	80	225	1100	1,700,000	
No. 4	2" x 6" wider	600	575	75	125	900	1,600,000	
Boards		500	475	70	125	800	1,500,000	
Common		400	400	65	125	700	1,400,000	
Timber		300	325	60	125	600	1,300,000	

NDS-1997

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### Adjustment Factors

NDS requires modification of the tabulated allowable stress values based on specific usage conditions as well as to account for stability:

- Duration of Load,  $C_D$
- Size Factor,  $C_F$
- Column Stability,  $C_P$
- Wet Use,  $C_M$

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### Load Duration Factor, $C_D$

- Wood can carrying greater maximum loads for shorter periods of time.
- Tabulated allowable stresses assume Live Load conditions (duration up to 10 years).
- Can use 60% increase for Wind and Earthquake loading.
  - Other codes use 1.33 increase
- 100% increase for impact loading
  - 2 sec or less.

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### Size Factor, $C_F$

Size Factor,  $C_F$

Tabulated bending, tension, and compression parallel to grain design values for dimension lumber 2" to 4" thick shall be multiplied by the following size factors:

Size Factors, $C_F$						
Grades	Width (depth)	$F_b$		$F_t$	$F_c$	
		Thickness (breadth)				
		2" & 3"	4"			
Select Structural, No. 1 & Btr. No. 1, No. 2, No. 3	2", 3" & 4"	1.5	1.5	1.5	1.15	
	5"	1.4	1.4	1.4	1.1	
	6"	1.3	1.3	1.3	1.1	
	8"	1.2	1.3	1.2	1.05	
	10"	1.1	1.2	1.1	1.0	
	12"	1.0	1.1	1.0	1.0	
	14" & wider	0.9	1.0	0.9		
Stud	2", 3" & 4"	1.1	1.1	1.1	1.05	
	5" & 6"	1.0	1.0	1.0	1.0	
	8" & wider	Use No. 3 Grade tabulated design values and size factors				
Construction & Standard	2", 3" & 4"	1.0	1.0	1.0	1.0	
Utility	4"	1.0	1.0	1.0	1.0	
	2" & 3"	0.4		0.4	0.6	

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### Wet Use Factor, $C_M$

Allowable stress values assume a moisture content not greater than 19%. If greater, must reduce allowable stresses as shown:

Wet Service Factors,  $C_M$

$F_b$	$F_t$	$F_v$	$F_{c\perp}$	$F_c$	E
0.85*	1.0	0.97	0.67	0.8**	0.9

\* when  $(F_b)(C_F) \leq 1150$  psi,  $C_M = 1.0$

\*\* when  $(F_c)(C_F) \leq 750$  psi,  $C_M = 1.0$

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### US&R Shoring

- Shoring capacity calculations based on Douglas Fir and Southern Pine.
- See StS FOG5 & SOG, Sect 4 - FAQ for other species.
- Based on NDS-1991.
- Allowable stresses may be increased up to 60% for emergency shoring.

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### Bending Members

$E = 1,400,000$  to  $1,600,000$  psi

$F_b = 1,500$  psi for 4x and 1,200 psi for 6x

$F_v = 95$  psi for 4x and 85 psi for 6x  
 (Increased by a factor of 2 in NDS-2001)

$F_b < M/S = (6M)/(bh^2)$       $F_v < (3V)/(2bh)$

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### Compression Members

Members are proportioned to preclude buckling:

$$F_a = 0.3 E (L/D)^2 \text{ (square posts)}$$

For  $E = 1,400,000$  psi and  $L/D = 25$ :

$$F_a = 420,000 \text{ psi} / (25)^2 = 672 \text{ psi}$$

Therefore:  $F_a = 672 \text{ psi} > F_{c\perp} = 625 \text{ psi}$

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## Section 2.0 Principles of Wood Design

### Bearing Failure in Wedges



$F_{c\perp} = 625 \text{ psi}$   
 $F_{c\perp} \times A_{\text{bearing}} =$   
 $625 \times 3.5 \times 3.5 =$   
 7,700 lbs per  
 bearing area  
**Use 8k (653 psi,**  
**round up)**  
 $672 \text{ psi} > 653 \text{ psi}$

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### Cribbing Bearing Failure



$F_{c\perp} = 500 \text{ psi}$   
 $F_{c\perp} \times A_{\text{bearing}} =$   
 $500 \times 3.5 \times 3.5 =$   
 6,125 lbs per bearing area  
**Use 6k**

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### Connections

- Usually steel fasteners that are subject to either:
  - Shear (lateral resistance) – Z
  - Withdrawal (tension) – W
- Design values for shear are based on mechanics approach while withdrawal values are empirical.
- Connection strength a function of wood (Specific Gravity) and fastener.

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### Connections

Four possible failure modes:

1. Uniform bearing failure in wood.
2. Non-uniform bearing failure in wood (fastener rotation without bending).
3. Single plastic hinge in fastener with wood bearing failure.
4. Two plastic hinges in fastener with wood bearing failure.

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### Raker Cleat



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### US&R Wire Nails – Lateral Resistance

Size	Diameter	Length	Z
8d common	0.128"	2-1/2"	90 lbs
16d vinyl coat	0.148"	3-1/4"	120 lbs
16d common	0.162"	3-1/2"	140 lbs

- Penetrate at least 12x dia to use full value.
- May increase value for metal side plates & duration of load (also plywood gusset?)
- **For US&R: 8d = 140 lbs, 16d vc = 190 lbs, 16d = 220lb ( 1.6 x increase – No Splits )**

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## **Section 2.0 Principles of Wood Design**

### **References**

1. *National Design Specifications for Wood Construction and Supplement*, American Forest & Products Association, 1991, 1997, and 2001 ([www.awc.org](http://www.awc.org)).
2. *Wood Handbook: Wood as an Engineering Material*, General Technical Report 113, Forest Products Laboratory, U.S. Dept. of Agriculture, 1999.
3. *Design of Wood Structures - ASD* (4th Edition), Breyer, D.E., Fridley, K.J., Cobeen, K.E., McGraw-Hill, 1999.

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